

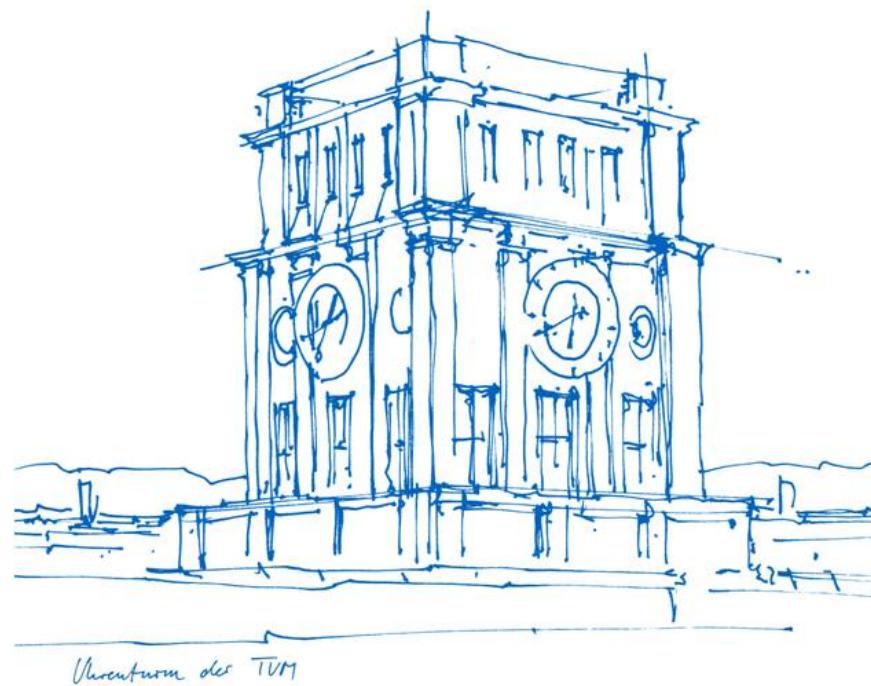
# Domain Decomposition from mechanical perspective

Prof. Daniel J. Rixen

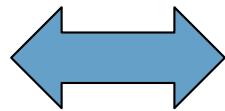
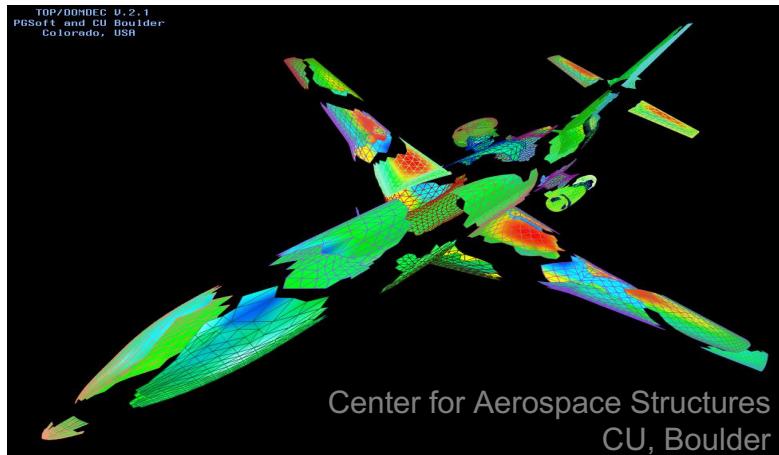
Kick-off training, January 2018  
Garching



European Training Network  
grant agreement No 721865



# Introduction



When splitting the problem in parts and asking different cpu's (or threads) to take care of subproblems, will the problem be solved faster ?

*FETI, Primal Schur (Balancing) method*

around 1990 .....

basic methods, mesh decomposer technology

1995-2000 .....

improvements

- preconditioners, coarse grids
- application to Helmholtz, dynamics, non-linear ...

2000-today .....

heterogeneous, dynamic, non-linear problems

Here the concepts are outlined using some mechanical interpretation.

## Content

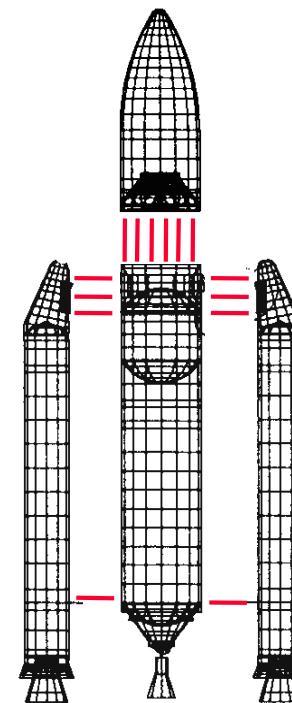
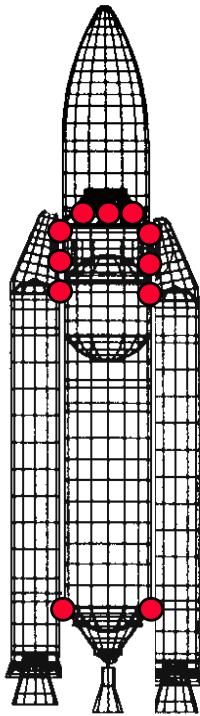
Part 1

1. Domain decomposition: Primal and Dual approaches
2. The FETI algorithm and preconditioners

Part 2

3. cyclic symmetry: harmonic decomposition
4. Quasi-cyclic problems and approaches
5. Project WP3 – 1 (ESR9)

## Domain Decomposition: Primal / Dual Assembly

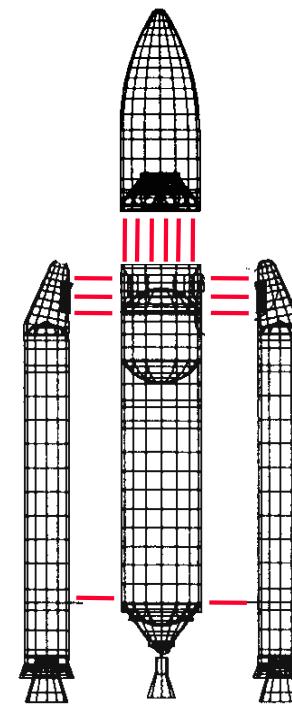
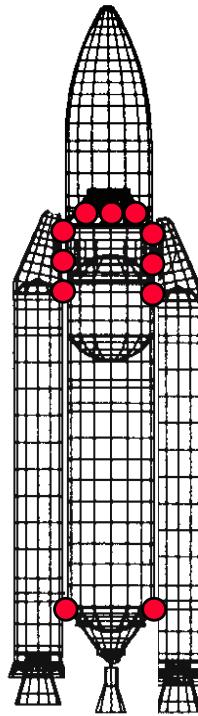


signed Boolean matrices

$$\begin{bmatrix} K^{(1)} & & 0 \\ & \ddots & \\ 0 & & K^{(N_s)} \end{bmatrix} \begin{bmatrix} u^{(1)} \\ \vdots \\ u^{(N_s)} \end{bmatrix} = \begin{bmatrix} f^{(1)} \\ \vdots \\ f^{(N_s)} \end{bmatrix}$$

$$\begin{bmatrix} K^{(1)} & 0 & B^{(1)T} \\ \ddots & \ddots & \vdots \\ 0 & K^{(N_s)} & B^{(N_s)T} \\ B^{(1)} \dots & B^{(N_s)} & 0 \end{bmatrix} \begin{bmatrix} u^{(1)} \\ \vdots \\ u^{(N_s)} \\ \lambda \end{bmatrix} = \begin{bmatrix} f^{(1)} \\ \vdots \\ f^{(N_s)} \\ 0 \end{bmatrix}$$

## Domain Decomposition: Primal / Dual Assembly

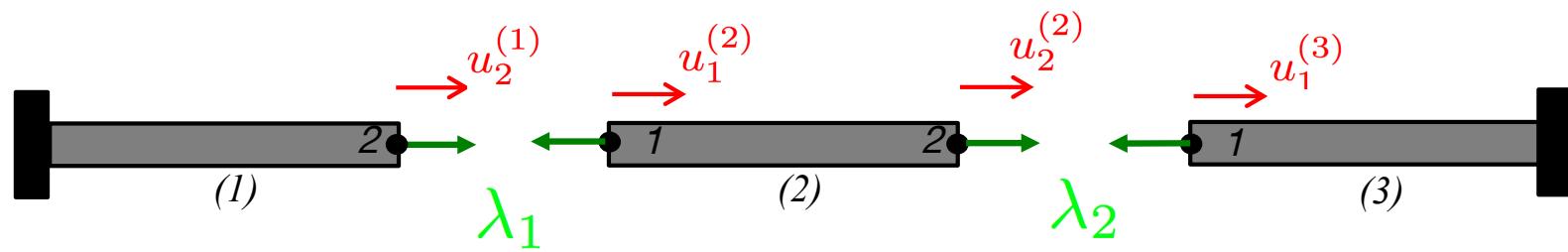


$$\begin{bmatrix} K^{(1)} & 0 \\ \vdots & \ddots \\ 0 & K^{(N_s)} \end{bmatrix} \begin{bmatrix} u^{(1)} \\ \vdots \\ u^{(N_s)} \end{bmatrix} = \begin{bmatrix} f^{(1)} \\ \vdots \\ f^{(N_s)} \end{bmatrix}$$

Block-diagonal notation

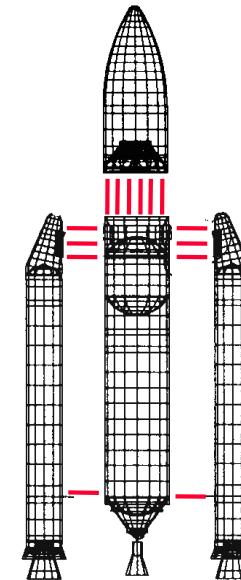
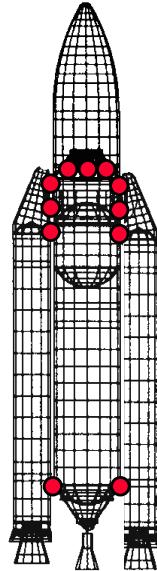
$$\begin{bmatrix} K & B^T \\ B & 0 \end{bmatrix} \begin{bmatrix} u \\ \lambda \end{bmatrix} = \begin{bmatrix} f \\ 0 \end{bmatrix}$$

- ▶ Example of bars.



$$\begin{bmatrix} \mathbf{K} & \mathbf{B} \\ \mathbf{B}^T & \mathbf{o} \end{bmatrix} \begin{bmatrix} \mathbf{u} \\ \lambda \end{bmatrix} = \begin{bmatrix} k^{(1)} & 0 & 0 & 0 \\ 0 & k^{(2)} & -k^{(2)} & 0 \\ 0 & -k^{(2)} & k^{(2)} & 0 \\ 0 & 0 & 0 & k^{(3)} \\ \hline 1 & -1 & 0 & 0 \\ 0 & 0 & 1 & -1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ -1 & 0 \\ 0 & 1 \\ 0 & -1 \\ \hline \mathbf{o} \end{bmatrix} \begin{bmatrix} u_2^{(1)} \\ u_1^{(2)} \\ u_2^{(2)} \\ u_1^{(3)} \\ \hline \lambda_1 \\ \lambda_2 \end{bmatrix}$$

## Iterative solution of interface problem

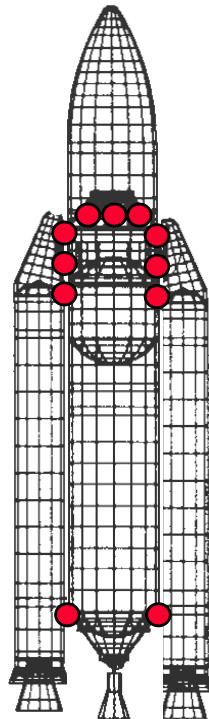


Iterate on interface dofs       $\mathbf{u}_b$   
|  
solve for internal dofs       $\mathbf{u}_i$   
|  
end (*when interface in equilibrium*)

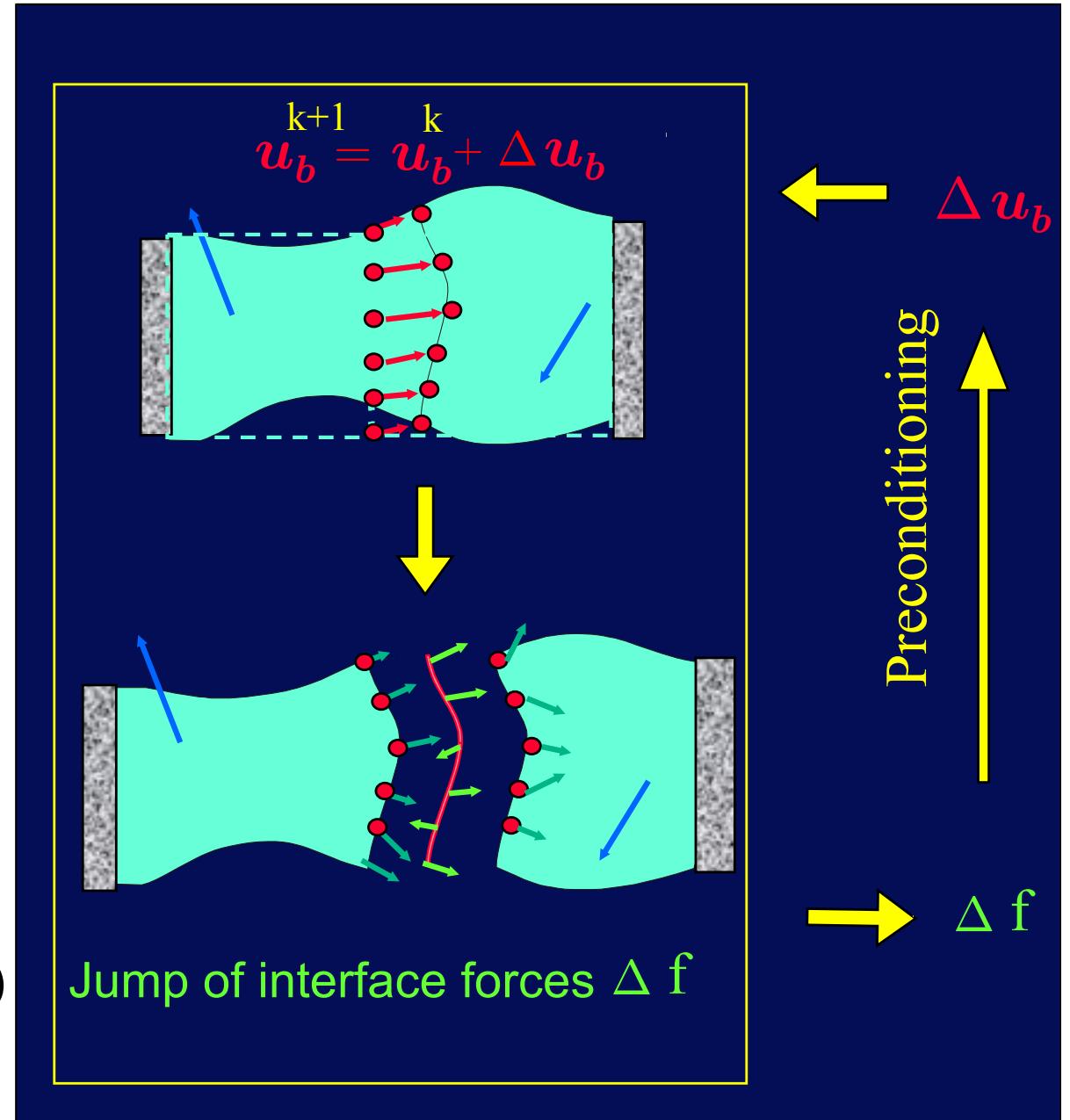
Primal Schur and BDD  
[Lelallec *et al.*, 91]

Iterate on interface forces       $\lambda$   
|  
solve for domain dofs       $\mathbf{u}$   
|  
end (*when interface compatible*)

FETI  
(Finite Element Tearing and Interconnecting)  
[Farhat- Roux, 91]

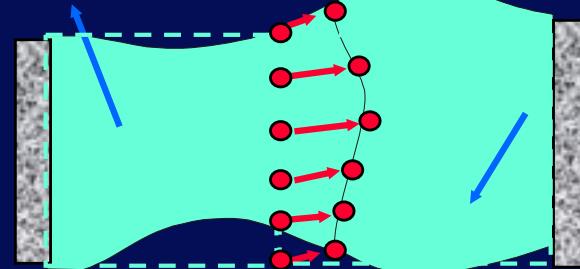


Iterate on interface dof  $u_b$   
 |      Solve for internal dof  $u_i$   
 end (when interface in equilibrium)

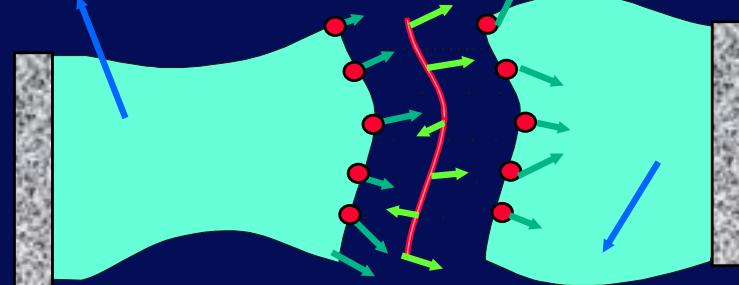


C.G. on  $\mathbf{u}$

$$\mathbf{u}_b^{k+1} = \mathbf{u}_b^k + \Delta \mathbf{u}_b$$



$$\Delta \mathbf{u}_b$$

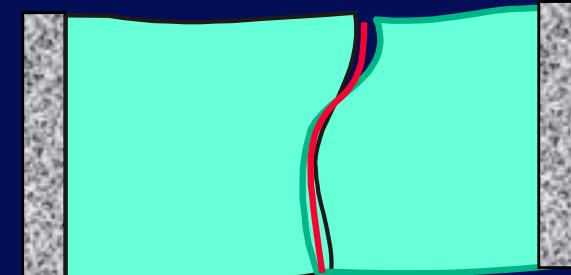


$$\Delta f$$

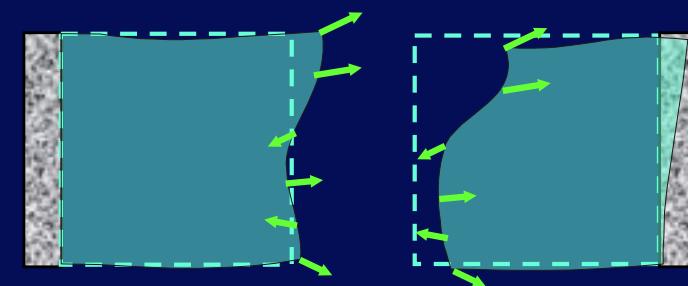
Jump of interface forces  $\Delta f$

Local Dirichlet

Preconditioning

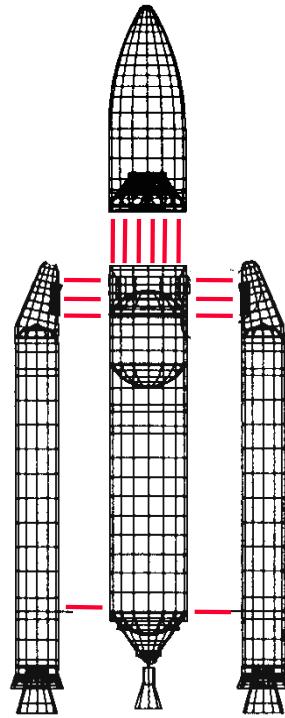


$$\Delta \mathbf{u}_b$$

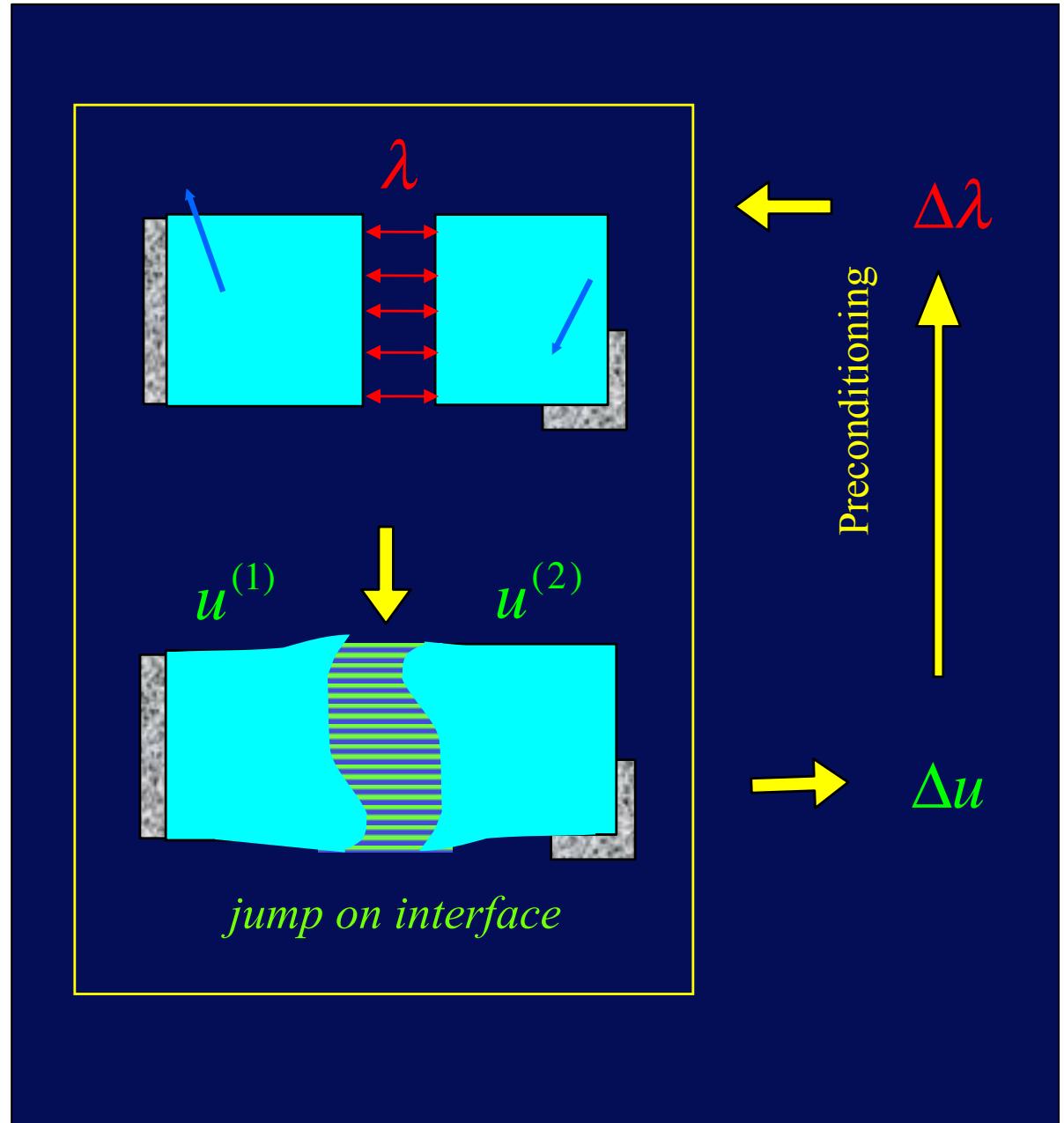


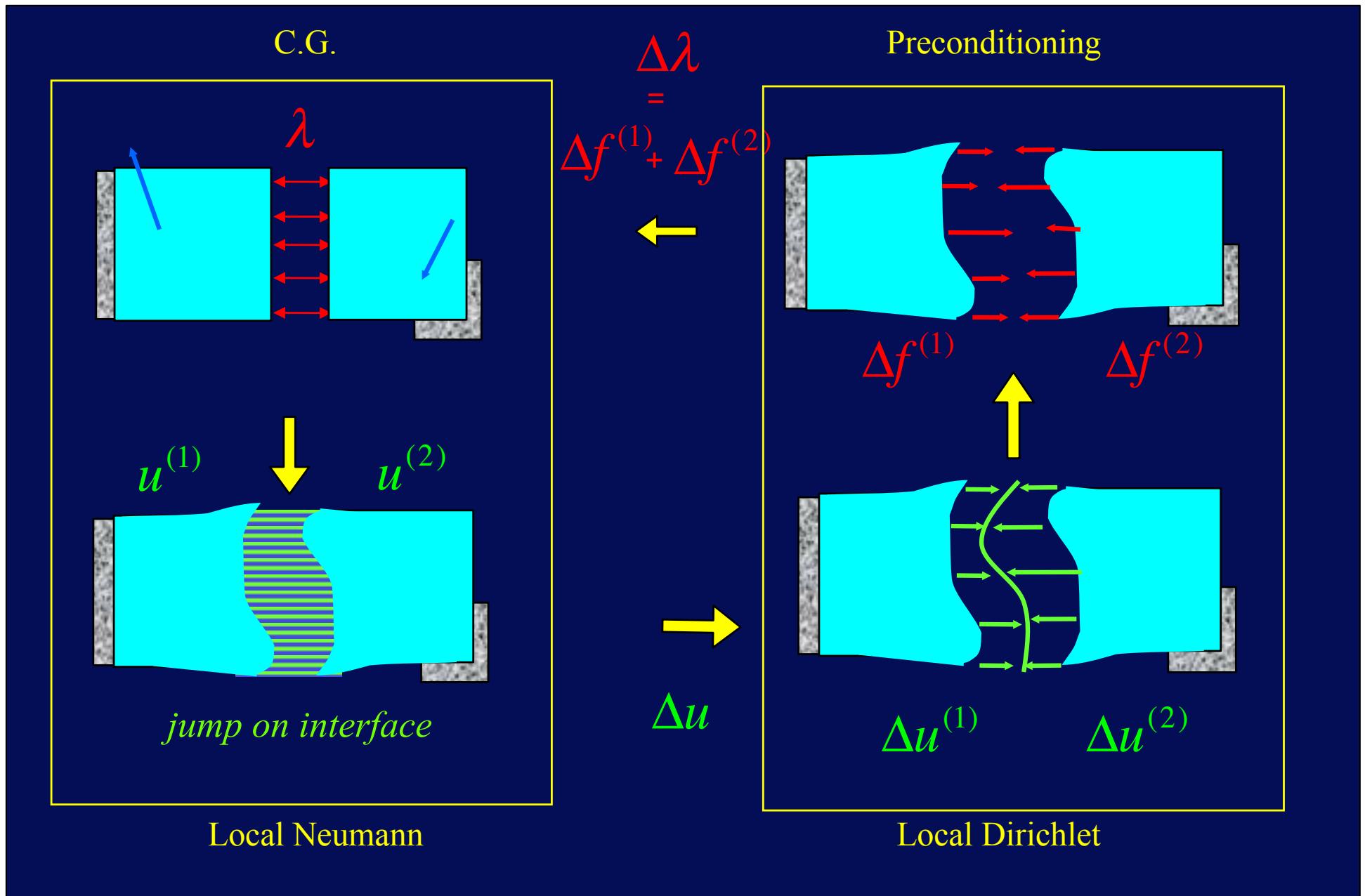
$$\Delta f$$

Local Neumann



Iterate on interface forces  $\lambda$   
|  
solve for domain dofs  $\mathbf{u}$   
|  
end (*when interface compatible*)





The primal and dual Schur complement approaches are very similar.

Most of the “tricks” used in the one method can be applied for the other.  
So which method to use is nearly a matter of religion ...

There exists some subtle differences such as

- treatment of cross-points (interface nodes on more than 2 domains)
- determination of an initial estimate

[ Klawonn 02, Gosselet *et al.* 03, Gosselet-Rey 06]

Here we outline only the dual approach (FETI)  
but one finds many publications on similar developments for the primal approach.

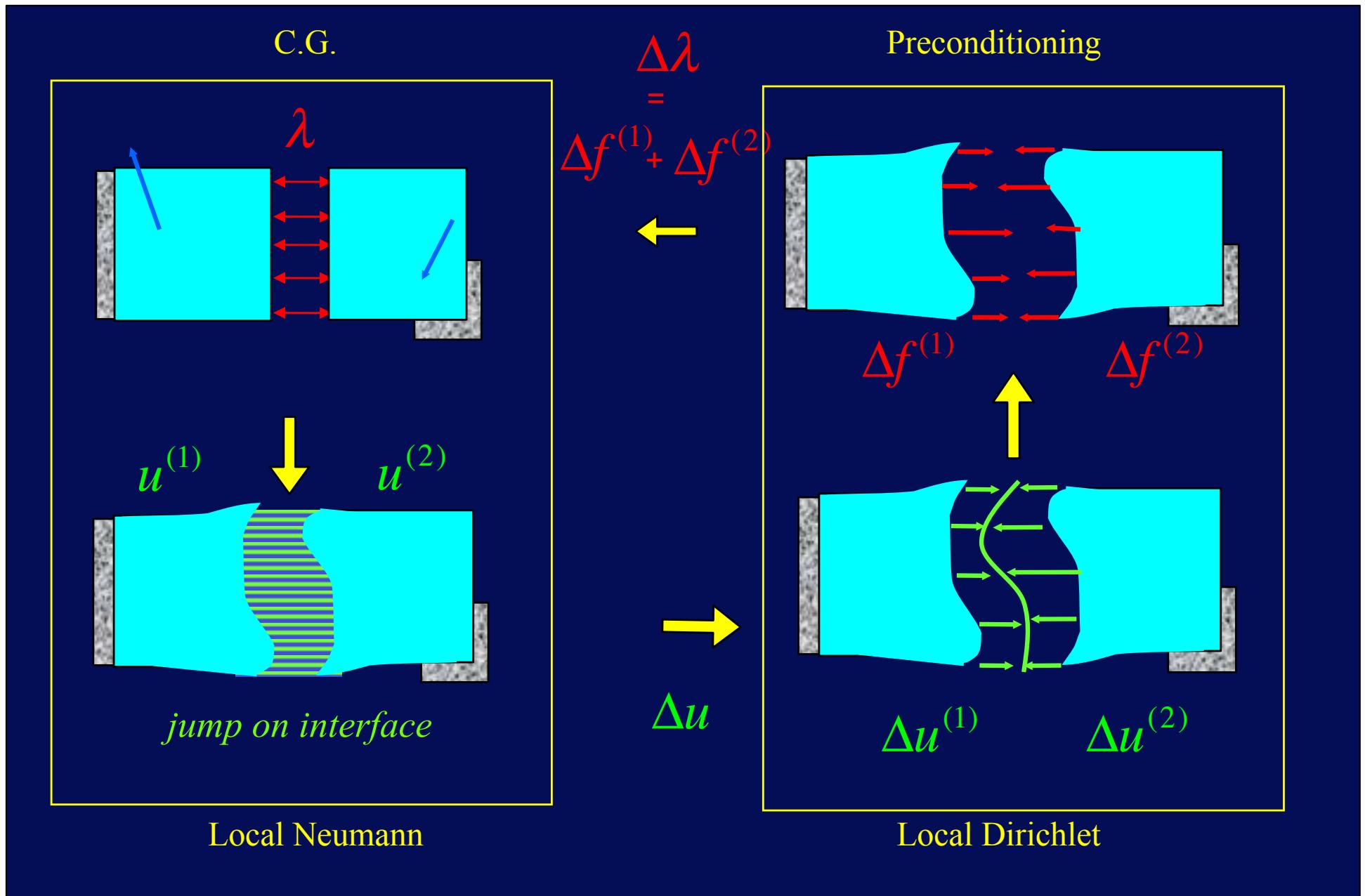
## Content

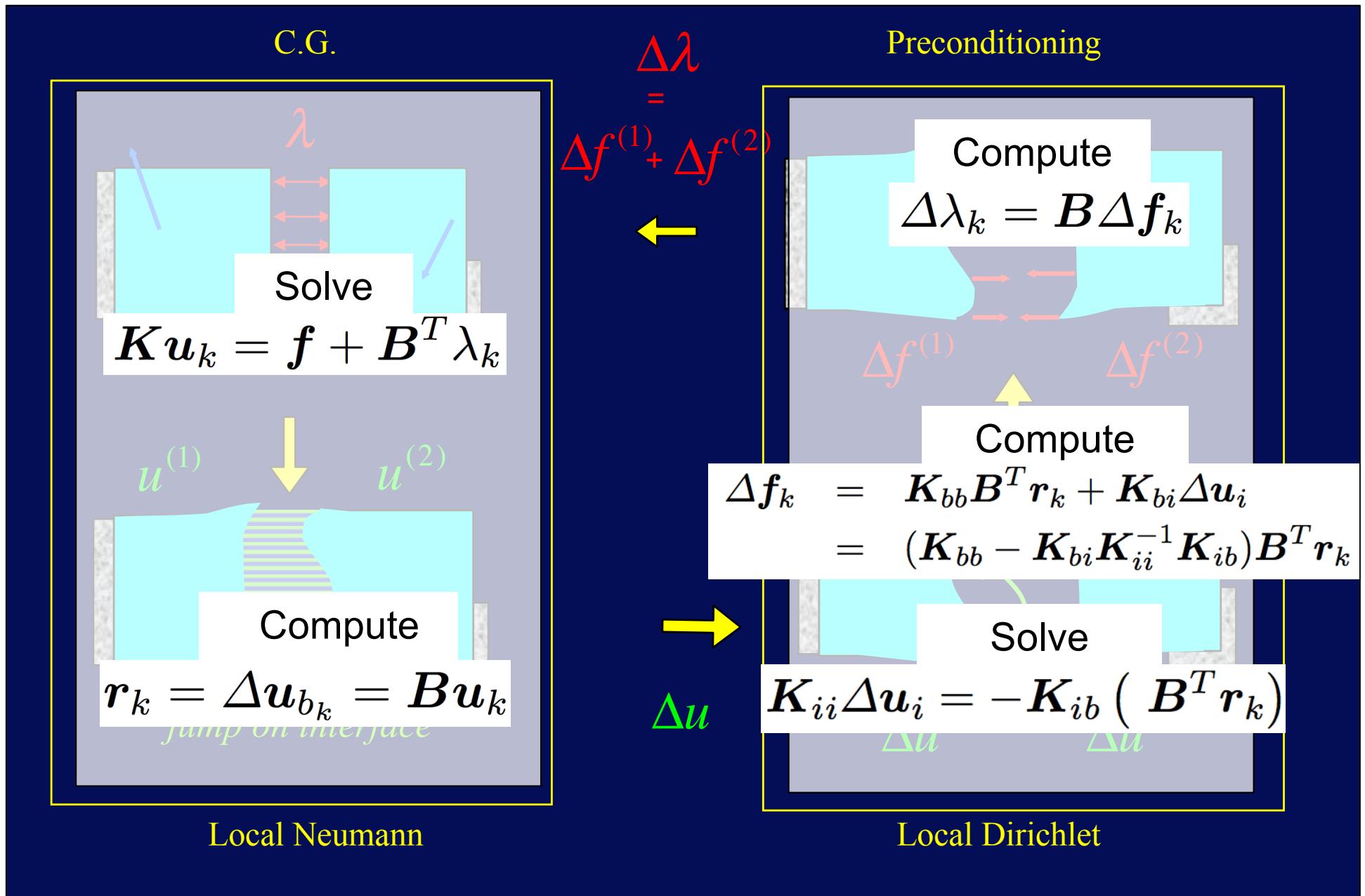
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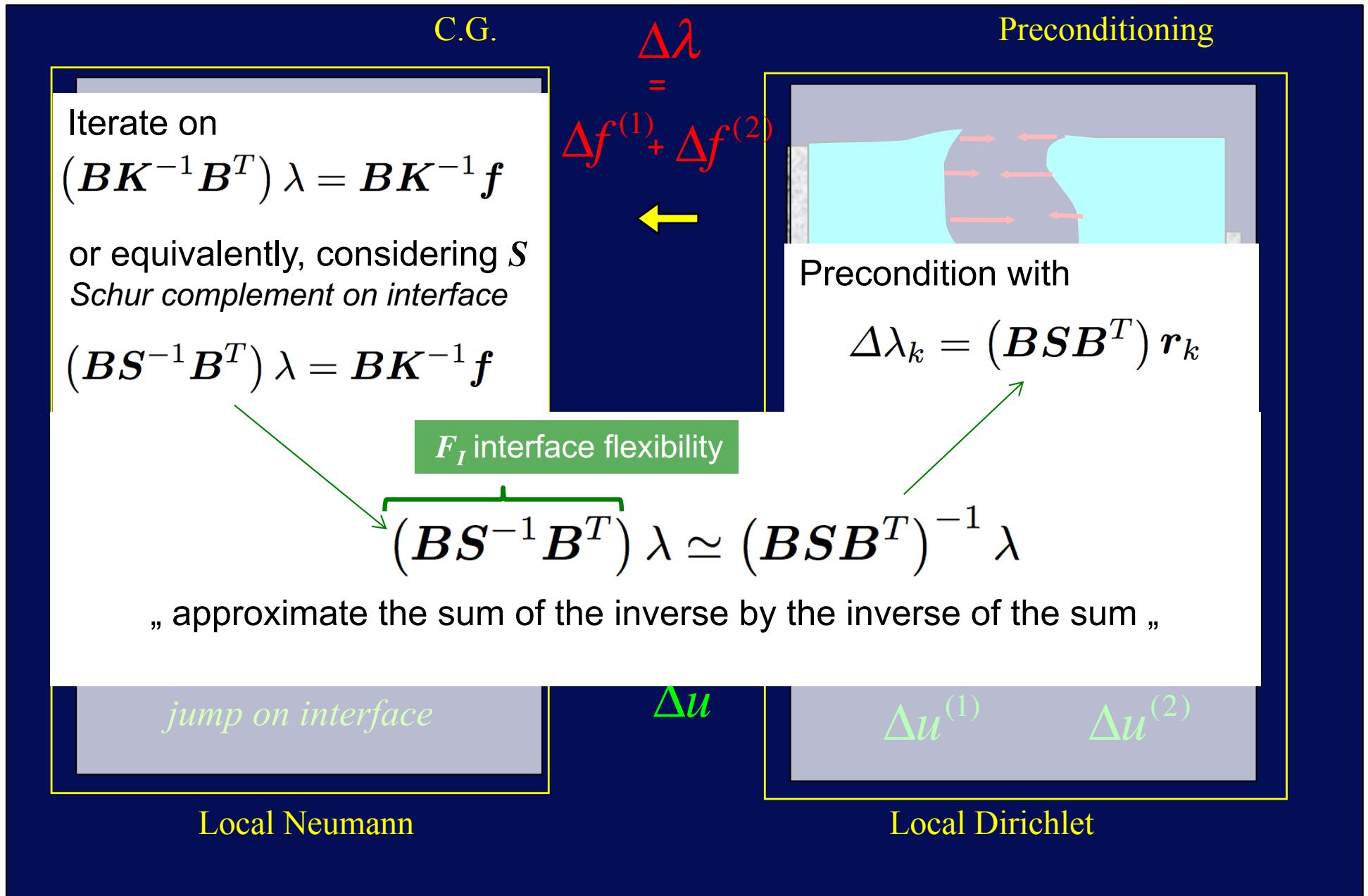
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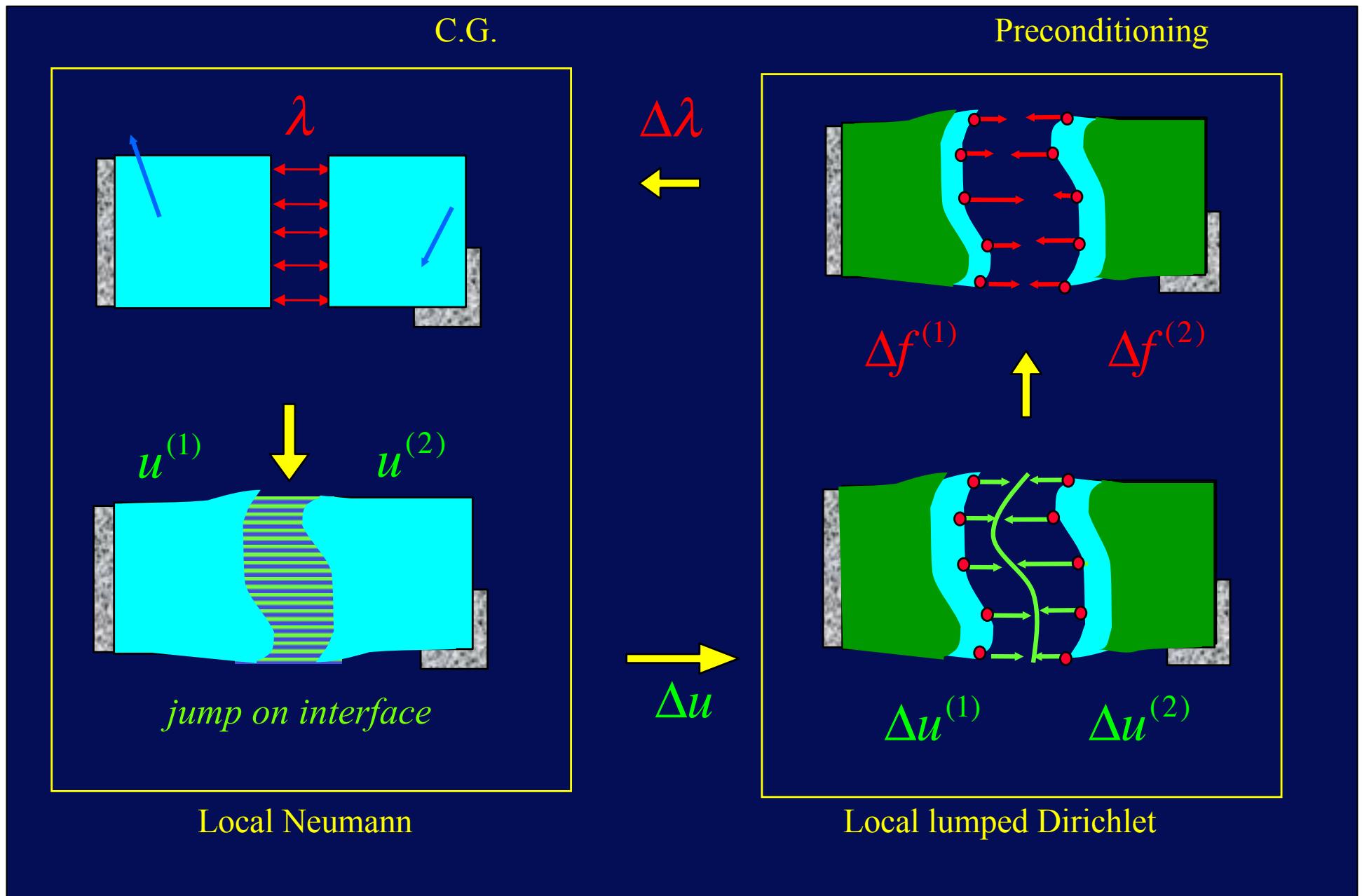
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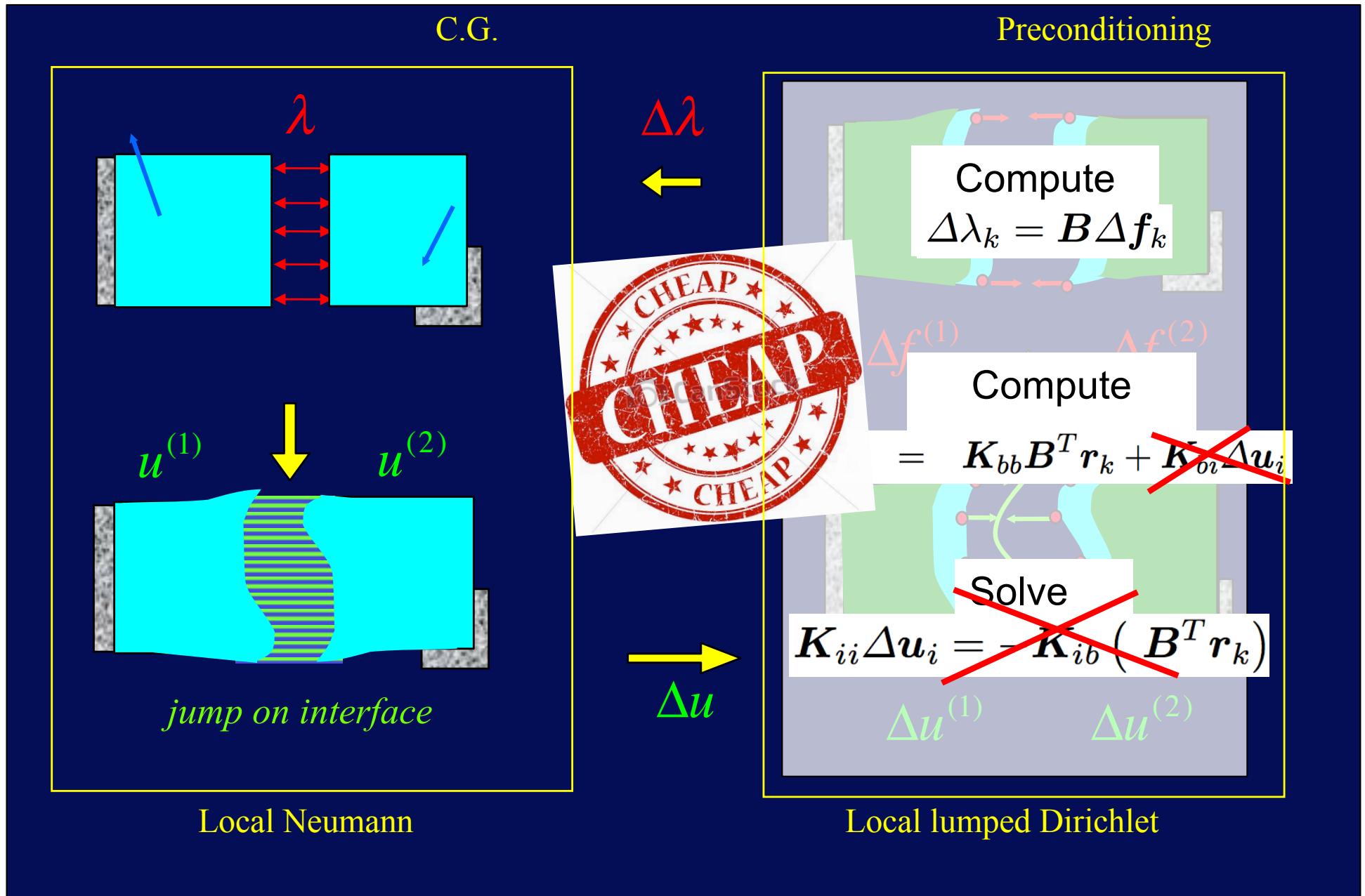
3. cyclic symmetry: harmonic decomposition
4. Quasi-cyclic problems and approaches
5. Project WP3 – 1 (ESR9)

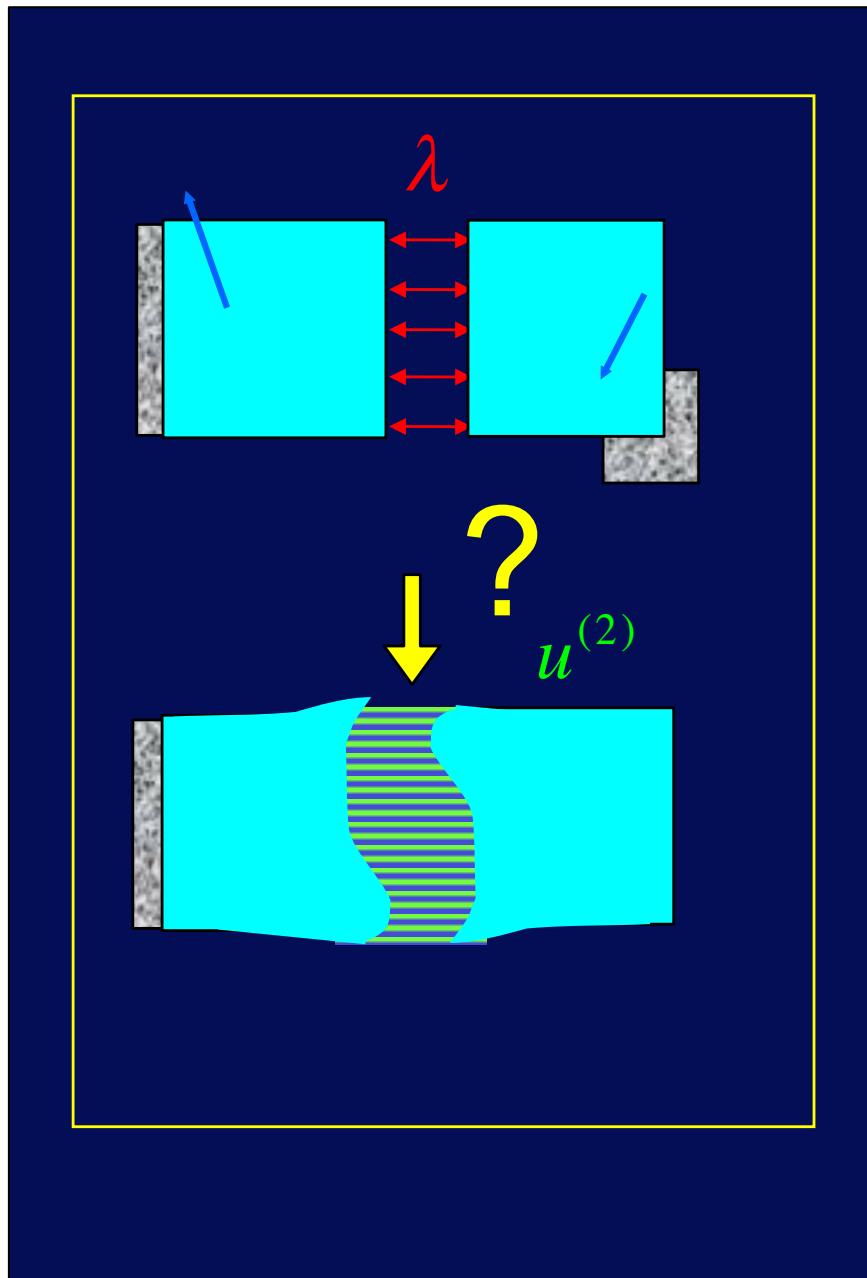












$$\begin{bmatrix} \mathbf{K} & \mathbf{B}^T \\ \mathbf{B} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \mathbf{u} \\ \boldsymbol{\lambda} \end{bmatrix} = \begin{bmatrix} \mathbf{f} \\ \mathbf{0} \end{bmatrix}$$

Not enough constraints  
Badly defined local problems  
Singular K

Requires to treat the rigid body motion of the domains separately and leads to a so-called **coarse grid**.  
(not discussed here)

## Content

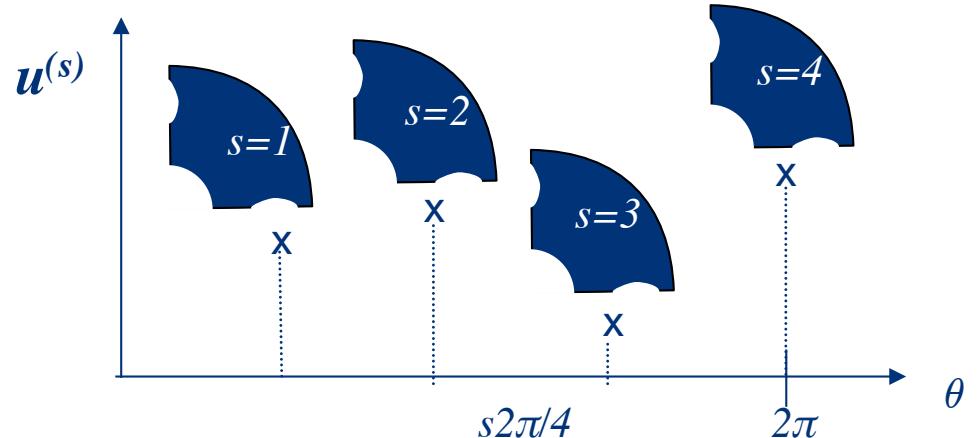
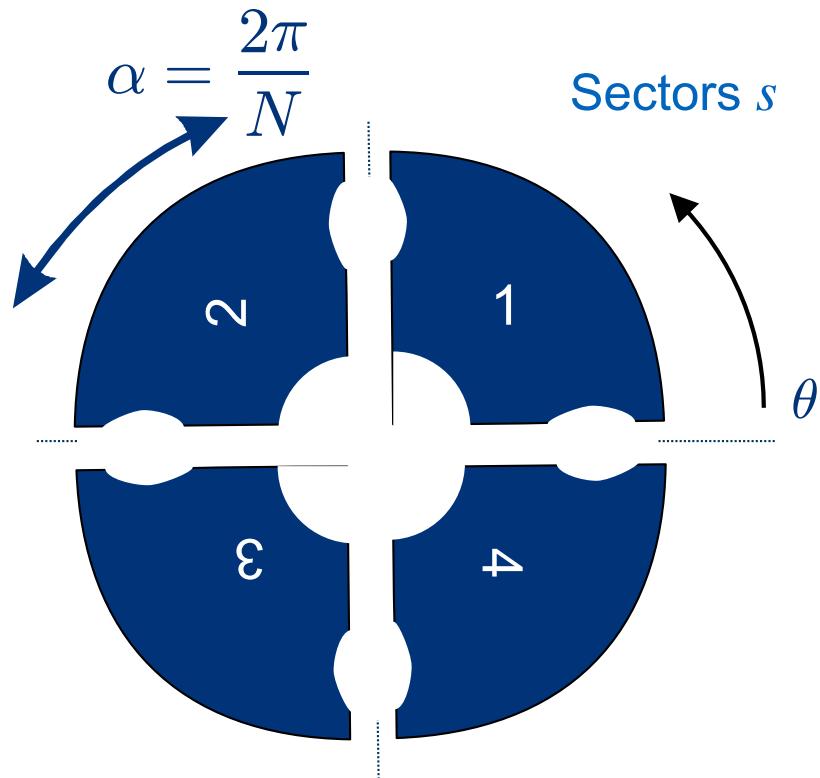
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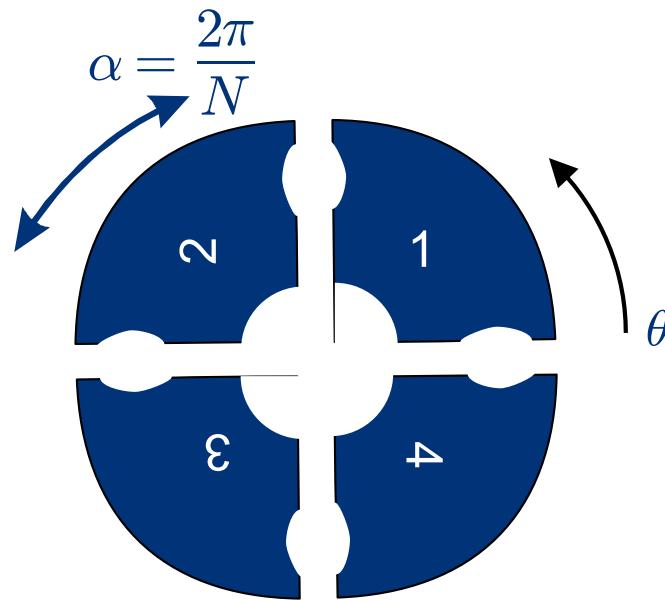
Part 2

3. Cyclic symmetry: harmonic decomposition
4. Quasi-cyclic problems and approaches
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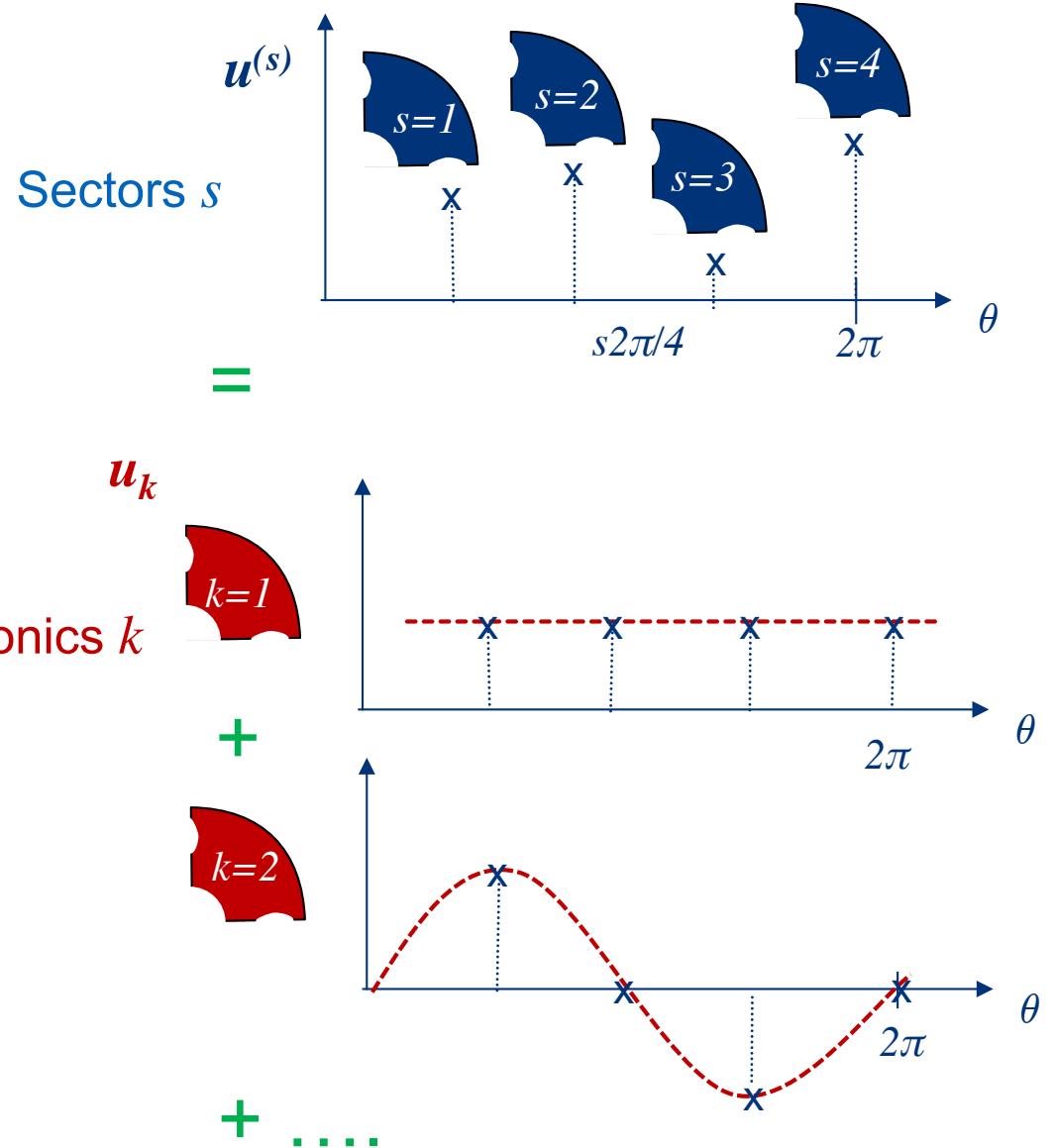
# Cyclic systems: harmonic decomposition



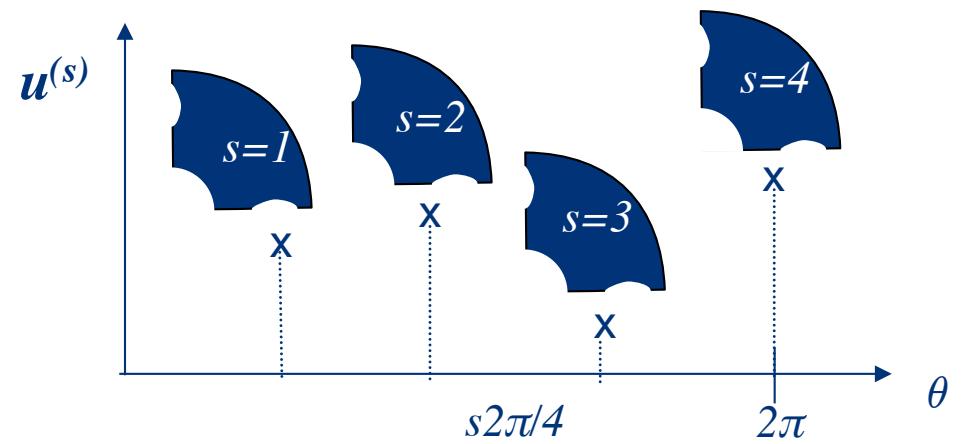
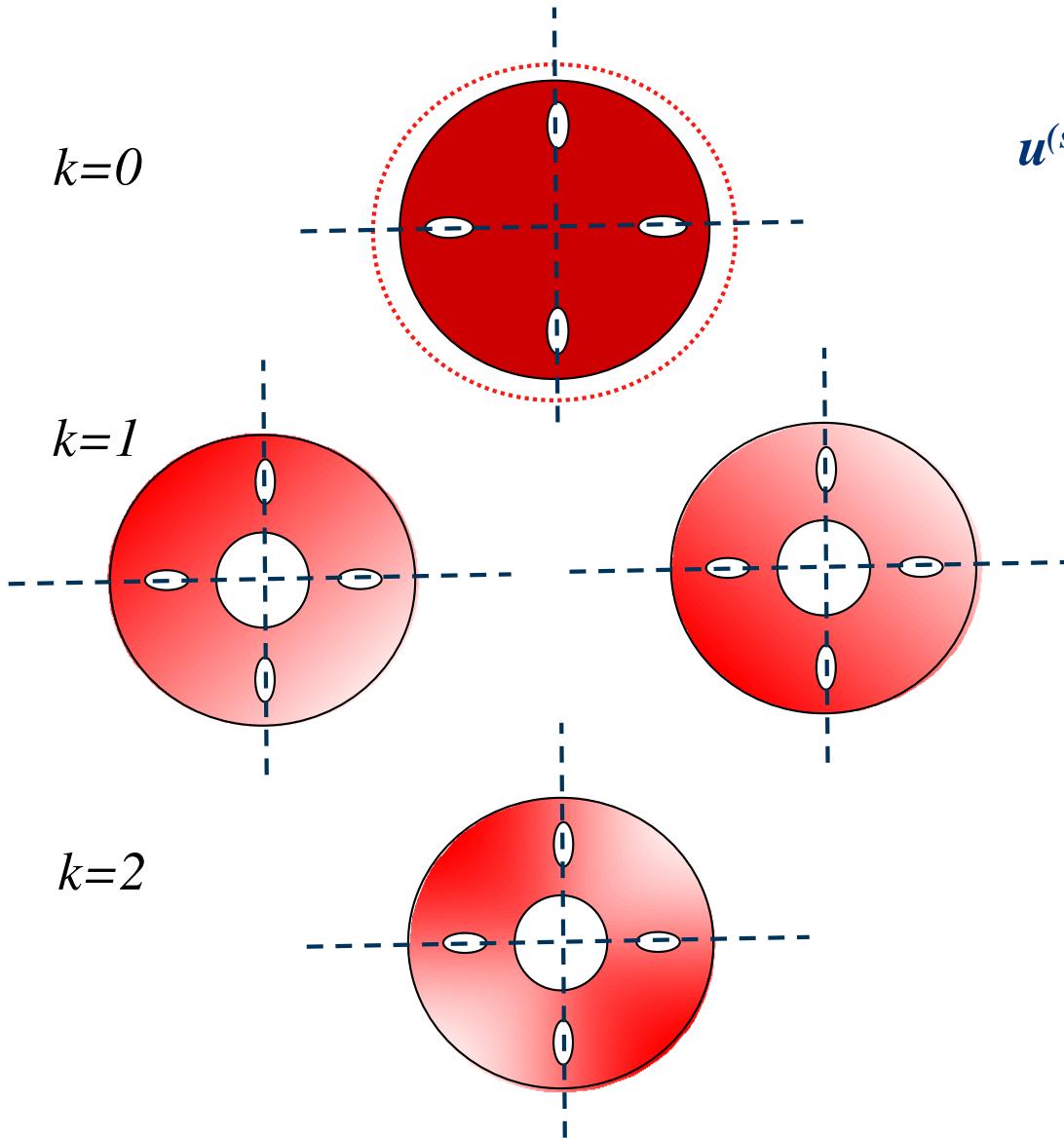
## Cyclic systems: harmonic decomposition



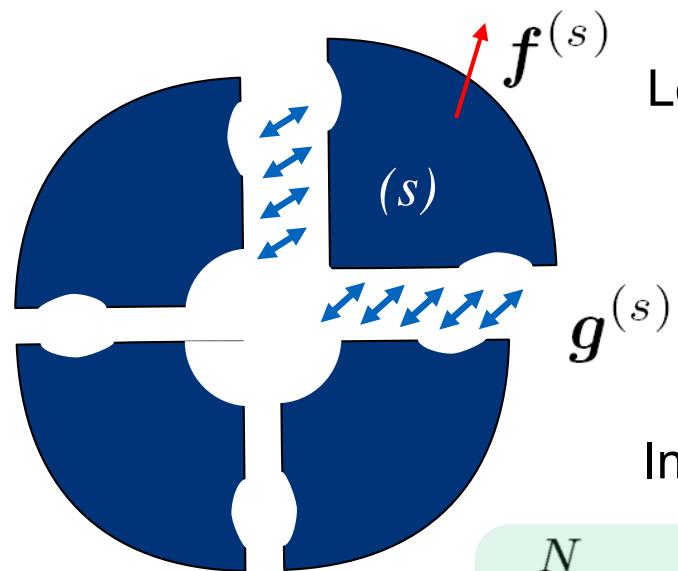
$$u^{(s)} = \sum_{k=0}^{N-1} u_k e^{-i \frac{k2\pi}{N} s}$$



## Cyclic systems: harmonic decomposition



$$u^{(s)} = \sum_{k=0}^{N-1} u_k e^{-i \frac{k2\pi}{N}s}$$



Local equilibrium

$$\cancel{M^{(s)}} \ddot{\mathbf{u}}^{(s)} + \cancel{K^{(s)}} \mathbf{u}^{(s)} = \mathbf{f}^{(s)} + \mathbf{g}^{(s)}$$

same local matrices for each sector  
but excitation does not need to be cyclic

Introducing the Fourier decomposition of sectors

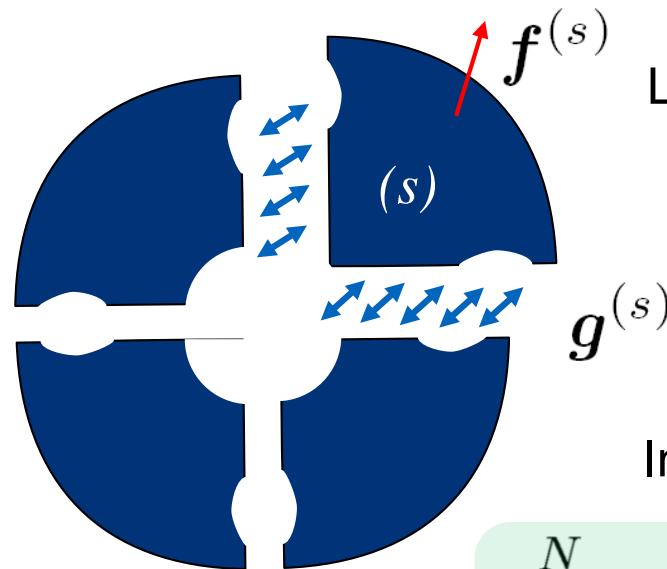
$$\sum_{s=1}^N e^{i \frac{r 2\pi}{N} s} \left[ M \ddot{\mathbf{u}}^{(s)} + K \mathbf{u}^{(s)} = \mathbf{f}^{(s)} + \mathbf{g}^{(s)} \right]$$

$$\sum_{k=0}^{N-1} \ddot{\mathbf{u}}_k e^{-i \frac{k 2\pi}{N} s}$$

$$\sum_{k=0}^{N-1} \mathbf{u}_k e^{-i \frac{k 2\pi}{N} s}$$

$$\sum_{s=1}^N e^{-i \frac{k 2\pi}{N} s} e^{i \frac{r 2\pi}{N} s} = 0 \text{ if } k \neq r$$

$\rightarrow M \ddot{\mathbf{u}}_k + K \mathbf{u}_k - \mathbf{j}_k \top \mathbf{y}_k = N \text{ if } k = r$



Local equilibrium

$$\cancel{M^{(s)}} \ddot{\mathbf{u}}^{(s)} + \cancel{\mathbf{K}^{(s)}} \mathbf{u}^{(s)} = \mathbf{f}^{(s)} + \mathbf{g}^{(s)}$$

same local matrices for each sector  
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Introducing the Fourier decomposition of sectors

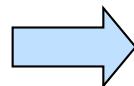
$$\sum_{s=1}^N e^{i \frac{r 2\pi}{N} s} \left[ M \ddot{\mathbf{u}}^{(s)} + \mathbf{K} \mathbf{u}^{(s)} = \mathbf{f}^{(s)} + \mathbf{g}^{(s)} \right]$$

$$\sum_{k=0}^{N-1} \ddot{\mathbf{u}}_k e^{-i \frac{k 2\pi}{N} s}$$

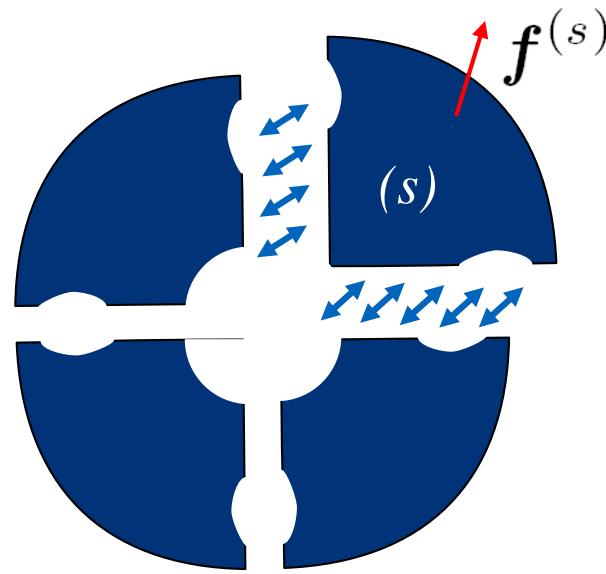
$$\sum_{k=0}^{N-1} \mathbf{u}_k e^{-i \frac{k 2\pi}{N} s}$$

From the orhtogonality of harmonic functions:

$$\begin{aligned} \sum_{s=1}^N e^{-i \frac{k 2\pi}{N} s} e^{i \frac{r 2\pi}{N} s} &= 0 \text{ if } k \neq r \\ &= N \text{ if } k = r \end{aligned}$$



$$M \ddot{\mathbf{u}}_k + \mathbf{K} \mathbf{u}_k = \mathbf{f}_k + \mathbf{g}_k$$



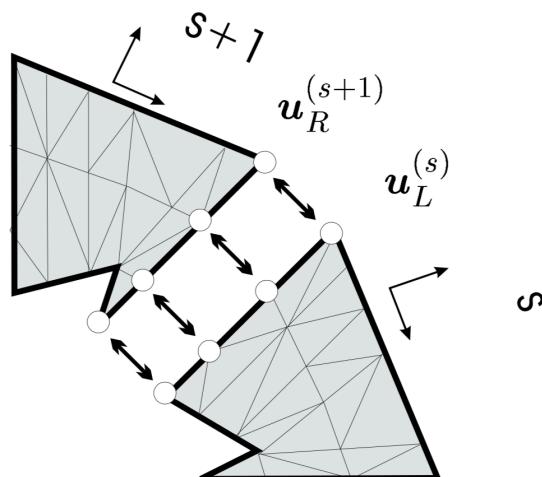
Uncoupled analysis of 1 sector for each harmonic

$$\mathbf{M}\ddot{\mathbf{u}}_k + \mathbf{K}\mathbf{u}_k = \mathbf{f}_k + \mathbf{g}_k$$

where  $\mathbf{f}_k = \frac{1}{N} \sum_{s=1}^N \mathbf{f}^{(s)} e^{i \frac{k2\pi}{N}s}$

$$\mathbf{g}_k = \frac{1}{N} \sum_{s=1}^N \mathbf{g}^{(s)} e^{i \frac{k2\pi}{N}s}$$

are the Fourier components of the forces



+ compatibility conditions on interface to determine  $\mathbf{g}_k$

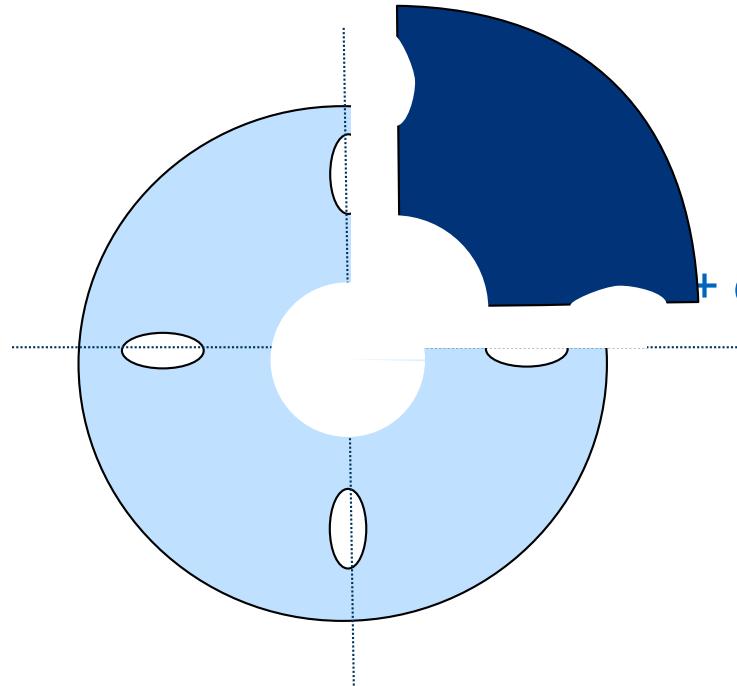
$$\mathbf{T}\mathbf{u}_L^{(s)} = \mathbf{u}_R^{(s+1)}$$

$$\mathbf{T}\mathbf{g}_L^{(s)} = -\mathbf{g}_R^{(s+1)}$$



$$\mathbf{T}\mathbf{u}_{k,L} = \mathbf{u}_{k,R} e^{-i \frac{k2\pi}{N}}$$

$$\mathbf{T}\mathbf{g}_{k,L} = -\mathbf{g}_{k,R} e^{-i \frac{k2\pi}{N}}$$



$$\mathbf{M}\ddot{\mathbf{u}}_k + \mathbf{K}\mathbf{u}_k = \mathbf{f}_k + \mathbf{g}_k$$

+ compatibility conditions on interface to determine  $\mathbf{g}_k$

.... and after rearrangement ...

$$\begin{aligned}
 & \begin{bmatrix} \mathbf{M}_{LL} + \mathbf{M}_{LR}\mathbf{T}e^{i\frac{k2\pi}{N}} + \mathbf{T}^T\mathbf{M}_{RL}e^{-i\frac{k2\pi}{N}} + \mathbf{T}^T\mathbf{M}_{RR}\mathbf{T} & \mathbf{M}_{Li} + \mathbf{T}^T\mathbf{M}_{Ri}e^{-i\frac{k2\pi}{N}} \\ \mathbf{M}_{iL} + \mathbf{M}_{iR}\mathbf{T}e^{i\frac{k2\pi}{N}} & \mathbf{M}_{ii} \end{bmatrix} \begin{bmatrix} \ddot{\mathbf{u}}_{k,L} \\ \ddot{\mathbf{u}}_{k,i} \end{bmatrix} \\
 & + \begin{bmatrix} \mathbf{K}_{LL} + \mathbf{K}_{LR}\mathbf{T}e^{i\frac{k2\pi}{N}} + \mathbf{T}^T\mathbf{K}_{RL}e^{-i\frac{k2\pi}{N}} + \mathbf{T}^T\mathbf{K}_{RR}\mathbf{T} & \mathbf{K}_{Li} + \mathbf{T}^T\mathbf{K}_{Ri}e^{-i\frac{k2\pi}{N}} \\ \mathbf{K}_{iL} + \mathbf{K}_{iR}\mathbf{T}e^{i\frac{k2\pi}{N}} & \mathbf{K}_{ii} \end{bmatrix} \begin{bmatrix} \mathbf{u}_{k,L} \\ \mathbf{u}_{k,i} \end{bmatrix} \\
 & = \begin{bmatrix} \mathbf{f}_{k,L} + \mathbf{T}^T\mathbf{f}_{k,R}e^{-i\frac{k2\pi}{N}} \\ \mathbf{f}_{k,i} \end{bmatrix}
 \end{aligned}$$

Uncoupled analysis of 1  
sector for each harmonic  
(commonly available in commercial codes)

## Content

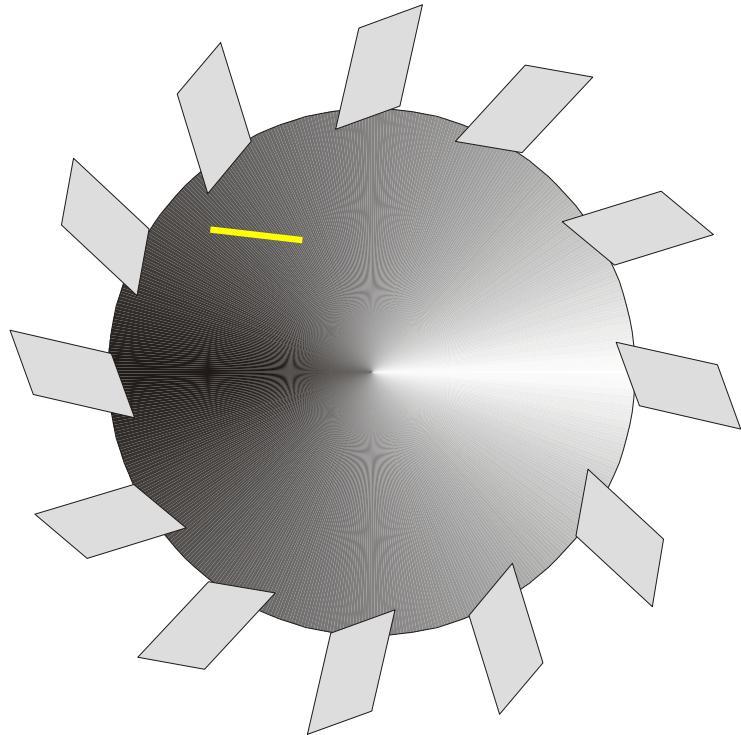
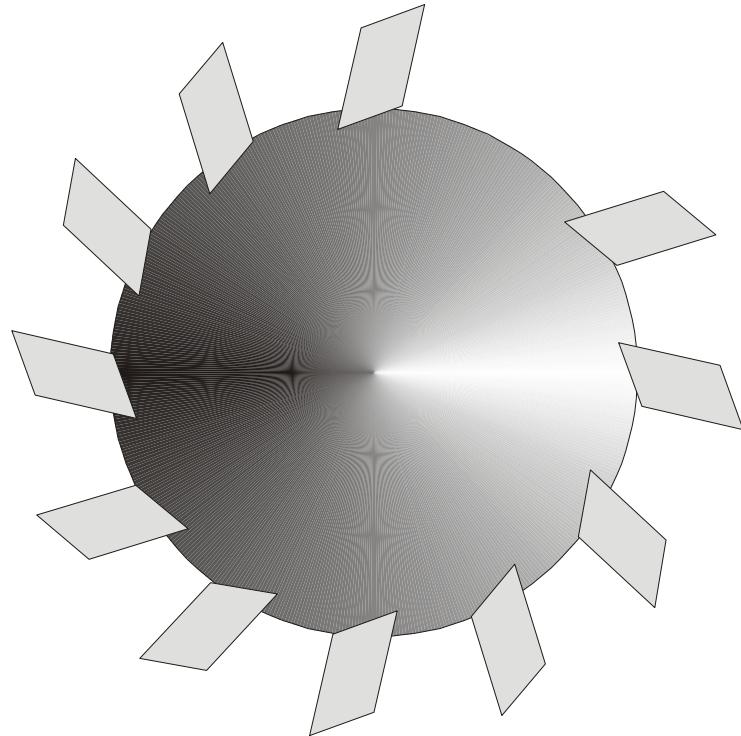
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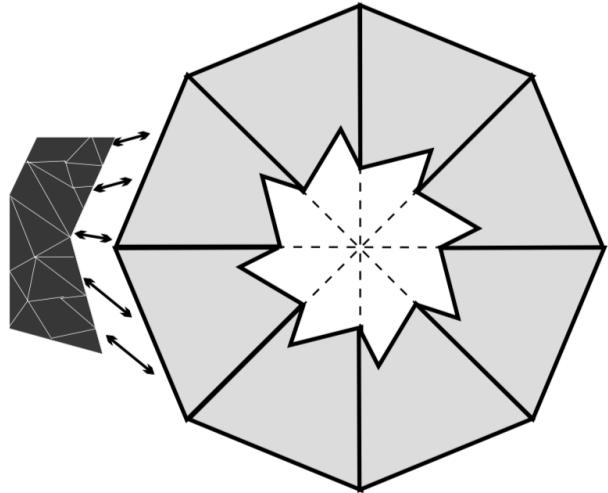
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But in practice, the cyclicity is not perfect



because of defaults, mistuning, dampers or local non-linearities

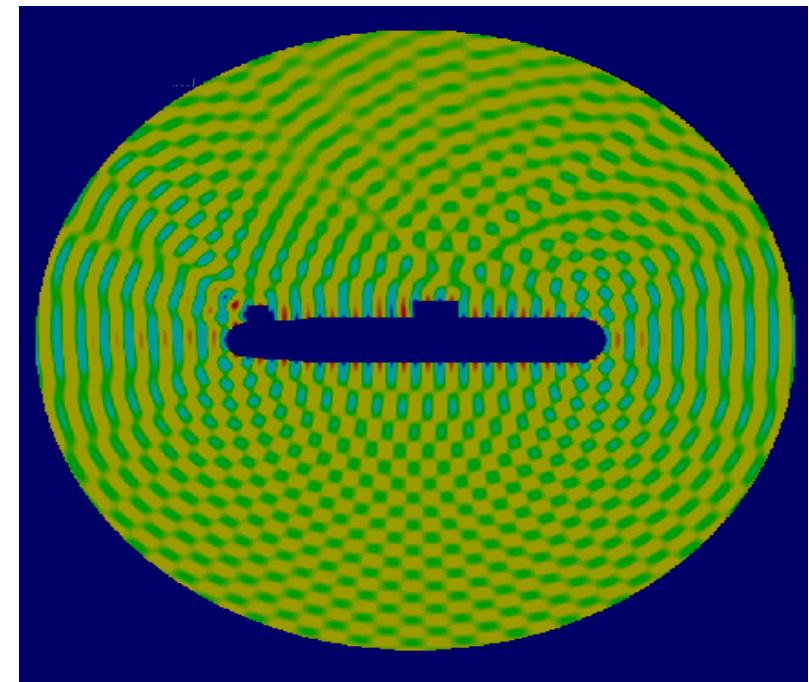
## Quasi-Cyclic systems: 2 domain decomposition approaches



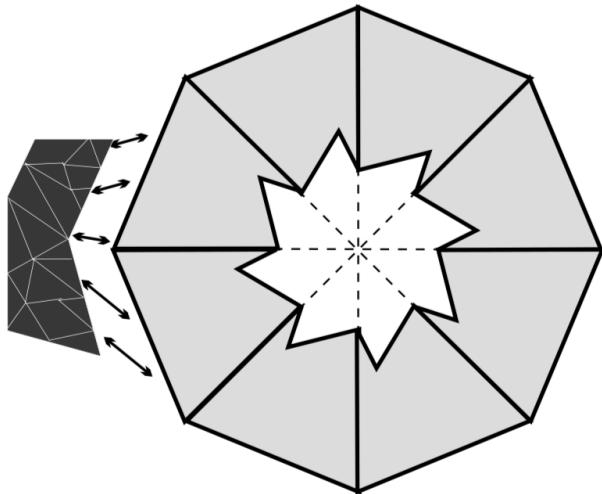
Method 1:

FETI iterations between cyclic part  
and non-cyclic part  
[Rixen 05]

originally proposed for axi-symmetric structures  
[Farhat 99, Farhat 02 ]

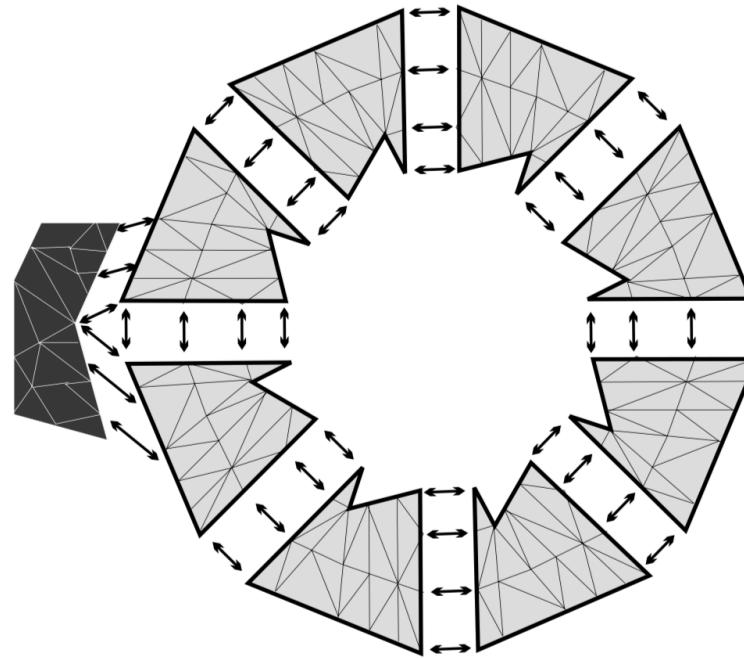


## Quasi-Cyclic systems: 2 domain decomposition approaches



Method 1:

FETI iterations between cyclic part  
and non-cyclic part  
[Rixen 05]

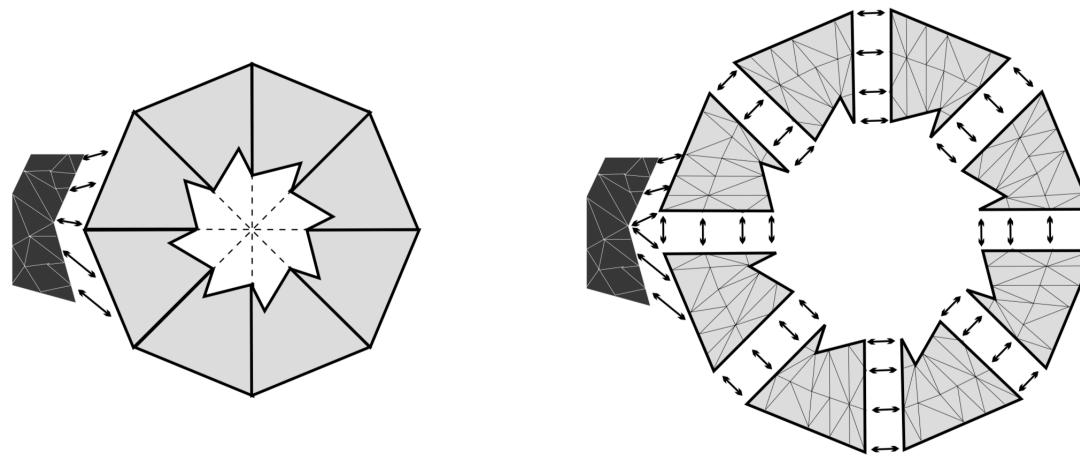


Method 2:

FETI applied considering all sectors  
as separate domains, and use the  
cyclicity in the preconditioner  
[Rixen 05]

## Research Project WP3 – 1 (ESR 9, Guilherme Jenovencio)

### Parallel scalability of the computation of quasi-cyclic turbine models using FETI-type methods



- Evaluate different FETI approaches for quasi-cyclic structures
- Possible extension with more advanced FETI techniques (FETI-DP, FETI-DP)
- Investigate the combination of FETI techniques and multi-harmonic analysis in case of local non-linearity (friction/contact)

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